VAV AIRFLOW CONTROL Reliable Without **Limitations?**



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21st National Conference on Building Commissioning

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Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.



Presentation Description

- 1. VAV Airflow Station...
- 2. ...testing at Factory Facilities
- 3. ...testing on projects
- 4. ...inaccuracy AFTER calibration
- 5. Medical Research facility example
- 6. Energy usage implications
- 7. Suggestions



Learning Objectives

At the end of this session, participants will be able to:

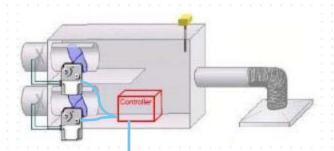
- Apply practical methods for evaluating VAV systems for proper operation and possible excessive energy use at minimum airflow.
- Communicate with HVAC professionals about VAV terminal units regarding performance and minimum airflow verification methodology.



VAV AIRFLOW CONTROL VAVs...What's the big deal anyway? Reliable Without Limitations?

...review project documents...





Building Automation System (BAS) guys...

...enter the VAV data into BAS application...



...upload BAS to each VAV controller

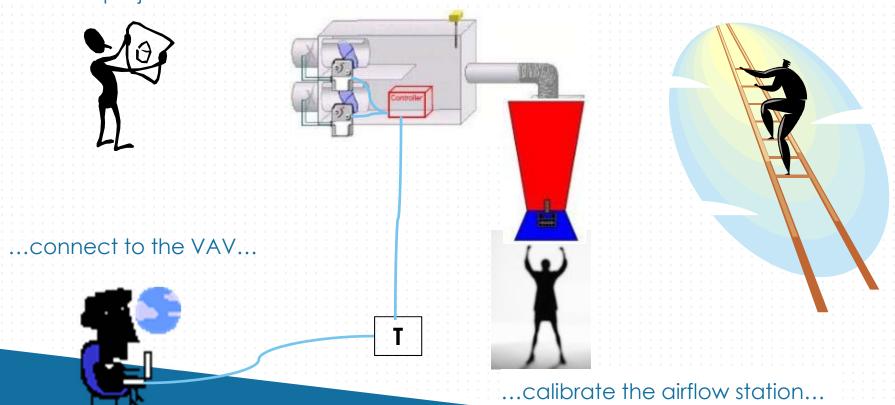


Reliable Without Limitations?

Testing Adjusting Balance (TAB) guys...

...review project information...

...proportionately balance the outlets...



Reliable Without Limitations?



...the VAV operates happily ever after...THE END...

...umm...isn't that true???

Why is it so
COLD in

here!!!



Why is it so LOUD in here!!!



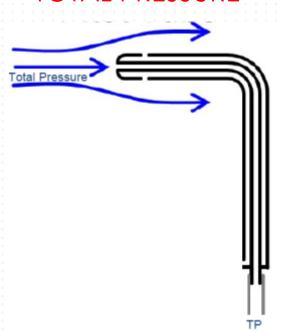
Why are these electrical & gas bills so EXTREME?!?!



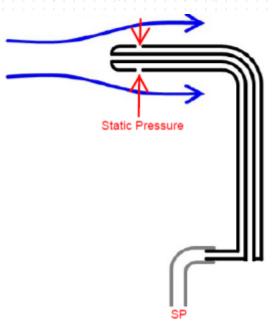
Reliable Without Limitations?

Pitot Tube Airflow Measurements

TOTAL PRESSURE



STATIC PRESSURE



Reliable Without Limitations?

Pitot Tube Airflow Measurements

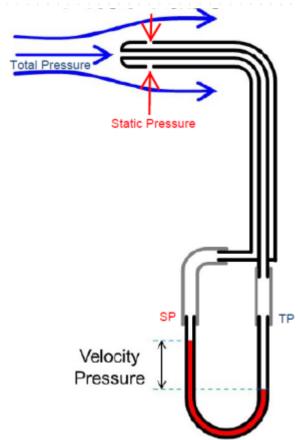
TOTAL PRESSURE

0 0

STATIC PRESSURE

_

VELOCITY PRESSURE (VP)

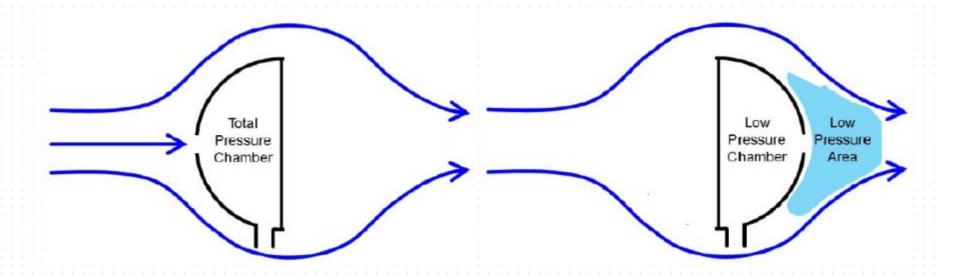


Reliable Without Limitations?

VAV Airflow Measurement...similar but different...

TOTAL PRESSURE

LOW PRESSURE



VAV AIRFLOW CONTROL VAV Airflow Sensor

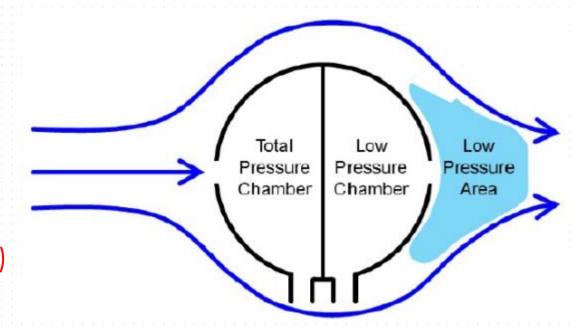
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Measurements

TOTAL PRESSURE

LOW PRESSURE

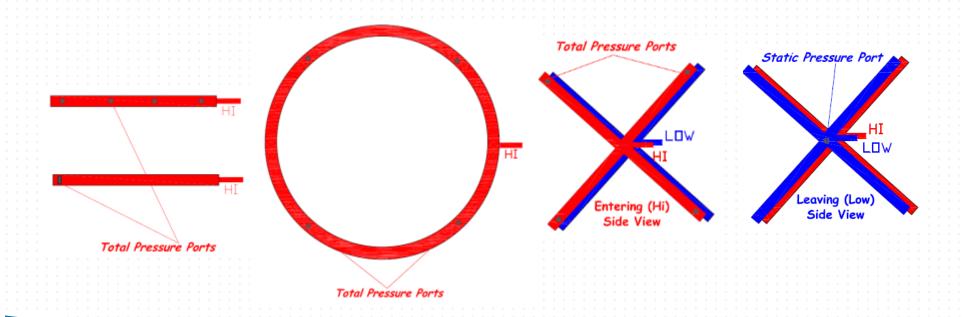
DIFFERENTIAL PRESSURE (ΔP)



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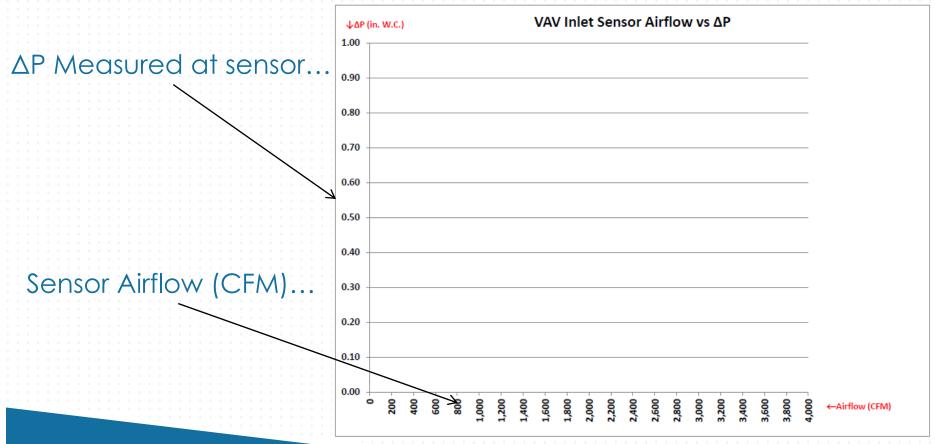
Examples of VAV Airflow Sensor Types

Examples of VAV airflow velocity sensors...



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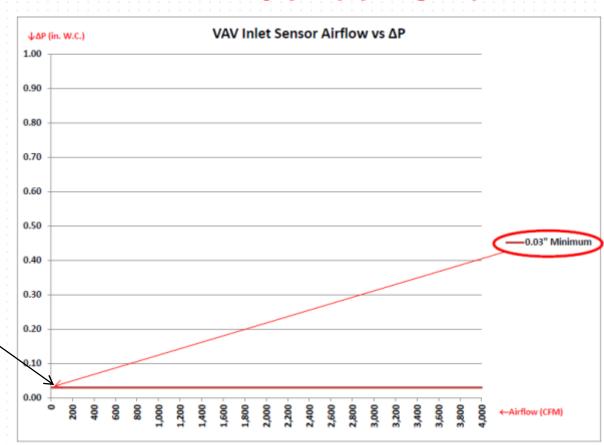
VAV Airflow Sensor Chart



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VAV Airflow Sensor Chart

Minimum measureable (Controllable) ΔP .

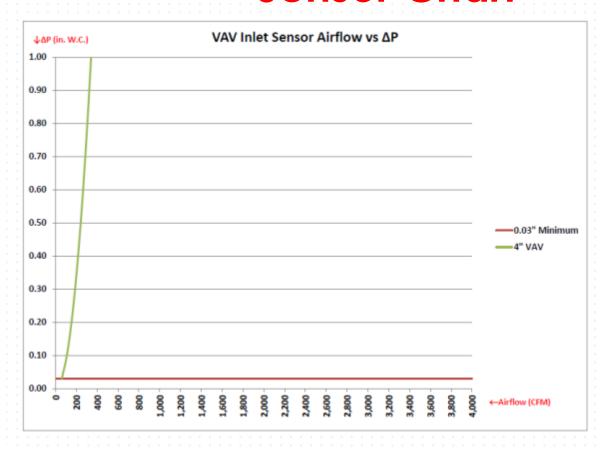


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VAV Airflow Sensor Chart

ΔP / CFM relationship...

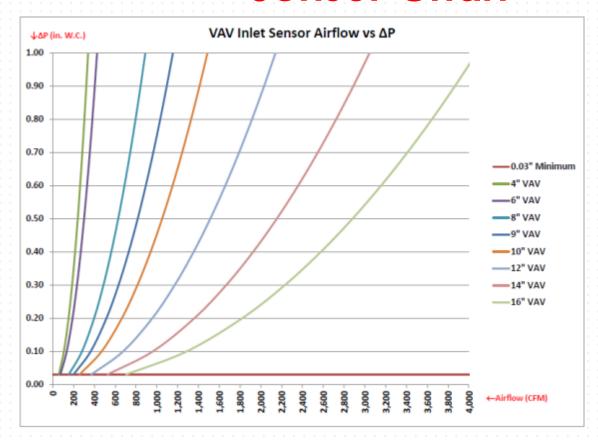
...4-inch VAV Inlet size...



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VAV Airflow Sensor Chart

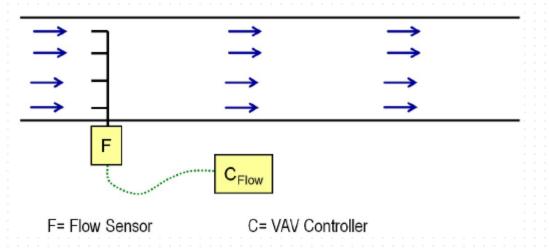
...through 16-inch VAV Inlet size...



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VAV Configuration deriving the Airflow Sensor Chart

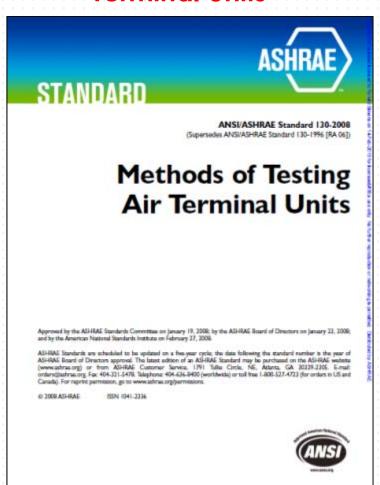
- No VAV Damper
- Airflow modulated by a fan with a VFD
- 3. Airflow measured at calibrated AFS.
- 4. Airflow pattern across sensor very laminar & consistent



Reliable Without Limitations?

VAV Manufacturers refer to ASHRAE 130-2008 for VAV testing Procedures...

Standard for Testing VAV Terminal Units



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Paragraph (5.6.1): "This test is intended to measure terminal unit air flow sensor output at various airflows (or velocities) for a specified duct static pressure. Its purpose is to determine the effects of the throttling device on flow sensor performance."

Standard for Testing VAV Terminal Units (Section 5.6)

he minimum operating pressure with installations other than those shown in Figures 3 and 4. These installation conditions shall be described in the last report.

5.3.2. Series flow fat-powered terminals shall have in airflow-measuring means, in accordance with Section 4.1, connected to a straight section of ductwork that is connected to the primary air inlet of the terminal, as shown in Figure 4. The inlet static pressure shall be mousered in accordance with Section 4.2 and referenced to atmospheric presents. An airflow-measuring means in accordance with Section 4.3 work that is connected to the terminal outlet. The static pressure resistance shall be measured in accordance with Section 4.2 and referenced to aimosphoric prossure. Airflow mary air damper valve in the fielly open position and with the fan delivering the desired nirflow against the desired static pressure resistance. Readings shall be taken after equilibrium has been established.

5.3.3 Parallel flow ten-powered and non-fan-powered tenninsis shall have an airflow-measuring means, in accordance with Section 4.3, connected to a situight section of ductwork that is connected to the primary air inlet of the terminal, as shows in Figure 6. A straight section of ductwork shall be connected to the discharge of the terroinal. The inlet static pressur- $(P_{\alpha \beta})$ and discharge static pressure $(P_{\alpha \beta})$ shall be recasured in accordance with Section 4.2. Inlet and discharge velocity prostates shall be calculated using nominal areas. Airflow and di forestal pressure $(\Delta P_a$ and $\Delta P_z)$ shall be recented with primary damper valve in the fully open position. The open condition of the fan in variable-volume fan-powered termina half he stated. Randings shall be taken after equilibrium has hors mishished

5.4.1 This test is intended to measure the leakage from the inside to the outside of the terminal unit. The terminal to be tested shall be installed as shown in Figure 3. This test method may be used to determine the caring lankage with installations that are set up other than as shown in Figure 5. These insta lation conditions shall be described in the test report.

5.4.2 An airflow-moustring mount, in accordance with Section 4.3, shall be connected to a simight section of duct work that is connected to the primary air inlet of the terminal The primary damper/valve shall be fully opened, and all other be excusared in accordance with Section 4.2. The primary air supply shall be increased until the desired static pressure obtained. Airflow and static pressure measurements shall be taken after equilibroum has been established. The castra leak age shall be reported to a clin (L/r) at y in. (Pa) static pressure. For parallel flow torsional units, the backdraft disoper leakage may be considered to be part of the easing leakage rid, as such, the induction port should not be scaled during the test. The leakage across the damper can be determined by scaling the induction port and calculating the difference in leakage during the two tests.

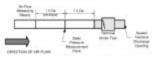
5.5.1 This test is intended to measure the leakage during penation of the terminal unit. The terminal to be tosted shall be installed as shown in Figure 6. This test method may be used to determine the dynamic leakage with installations that are set up other thus as shown in Figure 6. These installation conditions shall be described in the instruport,

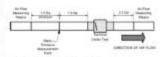
5.5,2 An airflow-measuring means in accordance will Section 4.3 shall be connected to a straight section of theiwork that is connected to the primary air inlet of the terms Section 4.3 shall be connected to a straight section of ductwork with a pressure-regulating device that is connected to shalf he set to achieve the desired indet static recessors at the desired primary airflow, and the conditions of all other outhere and inlete shall be stated. The desired discharge proshall be set. The relet and discharge static pressure shall be measured in accordance with Section 4.2. Airflow and static oute incuratements shall be taken after equilibrium has been established. The dynamic leakage is the difference butween the inlet airflow and the outlet airflow and shall be reported as a cfin (L/s) at y in. (Pa) static pressure

5.5.3 This test is intended to be run on a parallel flow to minal with the fan turned off.

ca.) This best is intended to measure terminal or New sensor output at various airflows (or velocities) for specified that static pressure. Its purpose is to determine the

in Figure 2. An sett Section 4.3 shall be connected to all primary inten. State presenges shall be recovered in accordance with Section 4.2.





ANSI/ASSIS All Standard 170 2008

Reliable Without Limitations?

Standard for Testing VAV Terminal Units (Section 5.6)

Question 1: Is there a completely open VAV damper in test unit while creating the published airflow sensor chart?

In correspondence I have been told "...no damper..." is present.

Question 2: No VAV damper means ASHRAE 130-2008, 5.6.1 testing is not performed?

No answer yet, still corresponding...

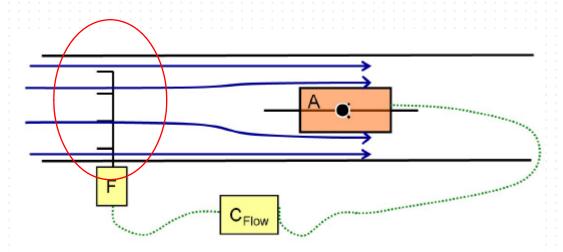
Question 3: Where is ASHRAE 130-2008, 5.6.1 testing data published?

No answer yet, still corresponding...

VAV Field Conditions

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Airflow pattern across airflow sensor of field installed VAV fairly laminar...



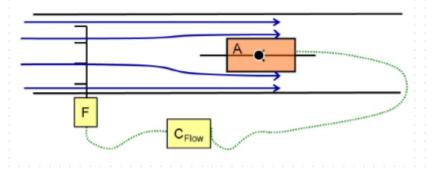
...Unfortunately...

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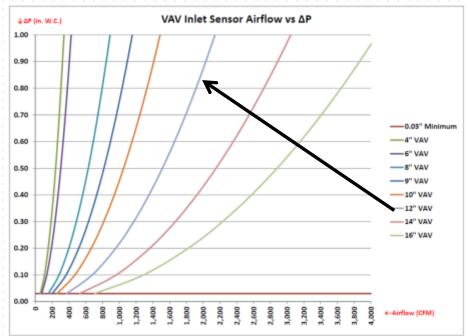
VAV Field Testing: Chart comparisons with Measured CFM

Field tests are perplexing...

Maximum CFM



12" VAV...

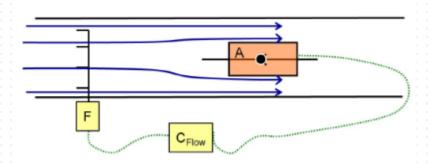


Reliable Without Limitations?

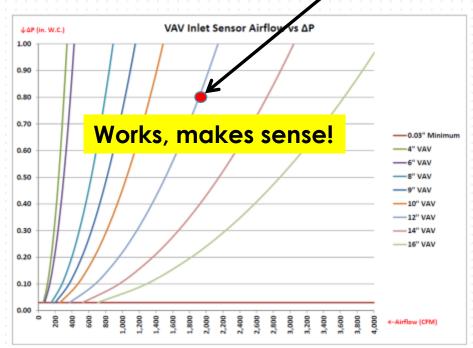
VAV Field Testing: Chart comparisons with Measured CFM

Field tests are perplexing...

Maximum CFM



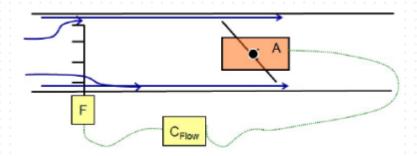
12" VAV, 1800 CFM @ 0.80 in. W.G.



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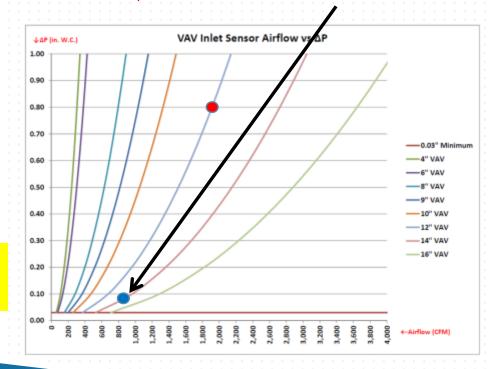
VAV Field Testing: Chart comparisons with Measured CFM

Minimum CFM



Why does the Minimum CFM plot on the 14" VAV curve?

12" VAV, 800 CFM @ 0.08 in. W.G.



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VAV Field Testing: Chart comparisons with Measured CFM

Attempted CFM / ΔP comparisons many times... LIMITED success...

...very LIMITED success...

CAUTION for the faint of heart...

"Traumatic" project experience follows...

VAV Field Testing:

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Accelerated Project Schedule

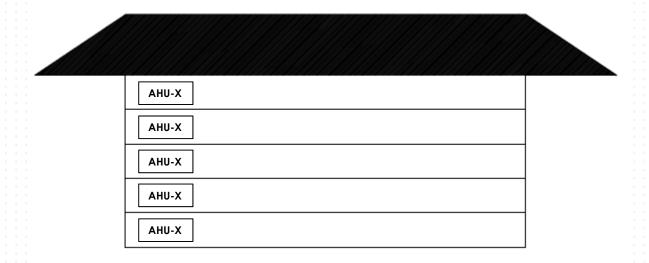
3 buildings...

Building 1 Building 2 Building 3

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VAV Field Testing: (Continued)

...each building had 5 floors...



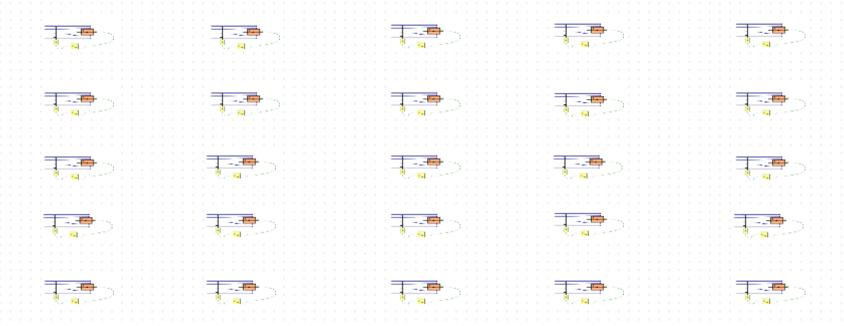
... dedicated AHU on each floor...

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VAV Field Testing:

Large DDC VAV Project with an Accelerated Project Schedule

...each AHU served 20-30 VAVs...



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VAV Field Testing:

"Unusual" Problem...

No Down-Duct Static control ...

...BUT...

...TAB needed to start to meet project schedule commitments!

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VAV Field Testing:

How TAB proceeded...

Closed 50% of VAVs on the floor we were working on...

...building down-duct static for other floor VAV calibration...

...calibrated & proportionately balanced VAVs...

...set completed VAV to control temperature (72°) moved to next VAV...

...until entire floor was completed.

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VAV Field Testing:

Why this would work

VAV's are "Pressure Independent".

Set final AHU down-duct static @ Operator Work Station (OWS)

VAV AIRFLOW CONTROL Reliable Without Limitations?

VAV Field Testing: Great Opportunity!

Kill two birds with one stone at OWS:

Identify hydraulically hardest to satisfy VAV(s) on each AHU...

Adjust AHU Down-Duct-Static setpoint to satisfy this VAV(s)

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VAV Field Testing:

What we failed to take into account...

VAV dampers @ Minimum CFM were 5-15% open...

...VAV dampers @ Maximum CFM were 20-30% open...

VAV Field Testing:

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...Later in our story @ OWS...

After 2 days at OWS...

... VAVs controlled Maximum Airflow with dampers 70-90% Open.

Concluded that it was time to:

Set AHU Minimum Outside Air...

Measure & document final AHU operational data...

...mere hours from project completion!

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VAV Field Testing:

...Spot check VAV airflow...

Zone airflow verification revealed...

Most VAV actual CFM was 20-30%...

HIGHER or LOWER than Design & BAS CFM!

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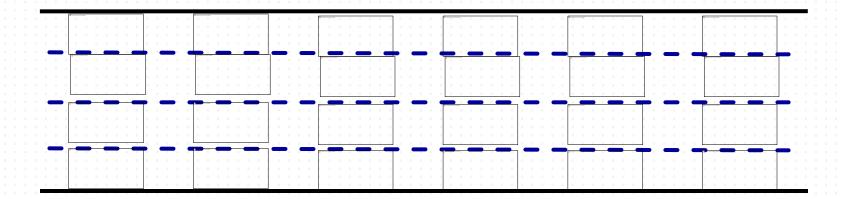
VAV Field Testing:

HUGE PROBLEM

WHAT HAPPENED?!?!

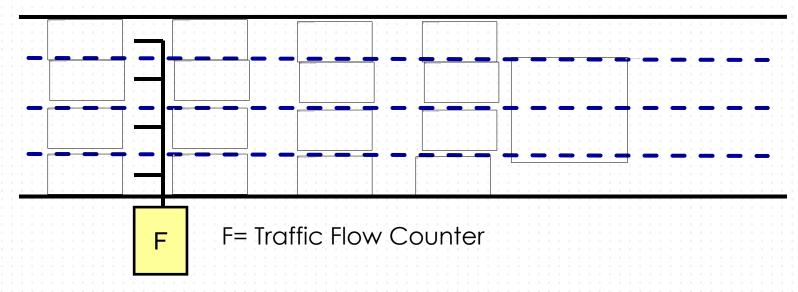
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Airflow in a duct is a lot like cars on a freeway...



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...add a traffic counting device...

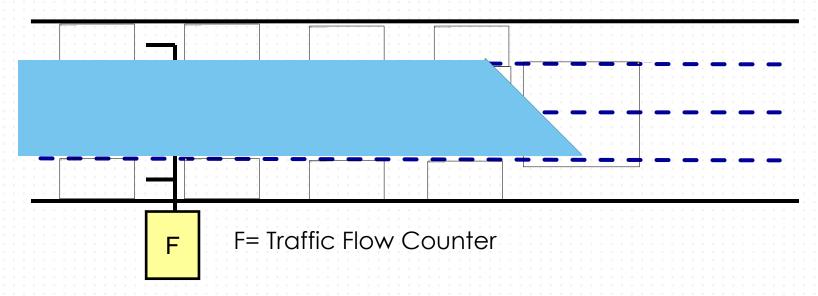


...traffic moves at a measurable rate...

...but what happens when...

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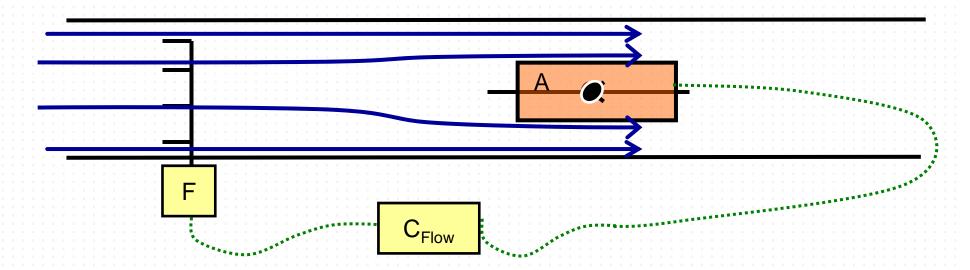
...big rig spin-out = traffic backup...



...creating a freeway "Dead-Zone"

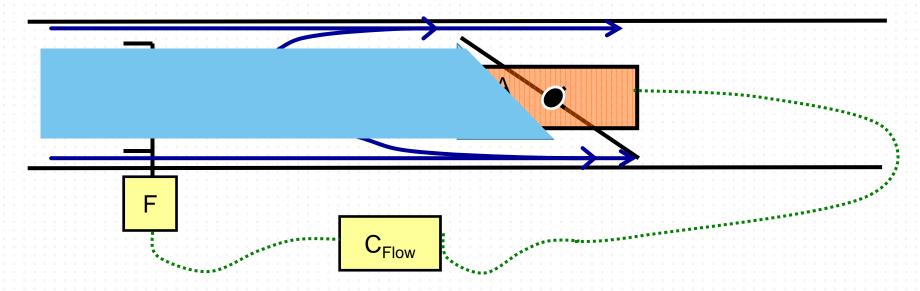
Reliable Without Limitations?

Airflow through airflow sensor with open VAV damper...no problem



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VAV damper closing is similar to the big rig spin-out...



...how far the "Dead-Zone" extends depends on the "traffic" or duct pressure behind the damper.

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Is this really THAT big of a deal?
How do you diagnose this issue?

EXAMPLE:

- 397,000 Square Foot Medical Research facility
- We'll look at 1 AHU (of many) supplying 100% OA through...
- Hot Deck (Steam Coil) and Cold Deck (CHW) at AHU down to...
- 62 Dual Duct VAVs, constant outlet airflow serving...
- Laboratories & Lab Support Administration areas

Our initial approach...

- Using the BAS, we began to evaluate zone performance.
- Rebalance had occurred 6-months earlier so...
- ...TAB report was in our hands.
- Began to look for "Targets of Opportunity" to allow us to...
- ...move to zone level with our instruments to verify system operation.

Typical VAV:

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NOBODY KNEW ANYTHING...

Design Flow Total = 3,015 CFM

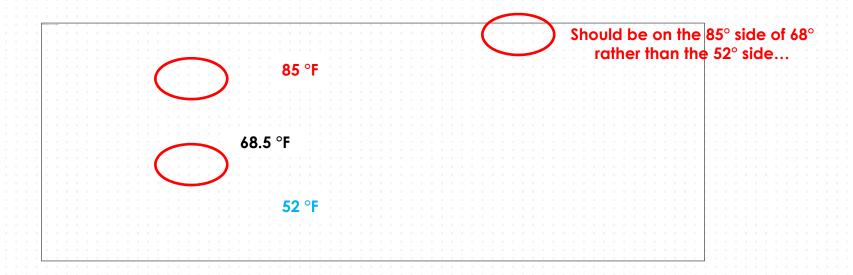
TAB calibrated Hot & Cold VAV controllers at 2,380 Max CFM but...

...did not document Minimum airflow calibration in the TAB Report...

... Max CFM discrepancy and lack of Min CFM documentation...

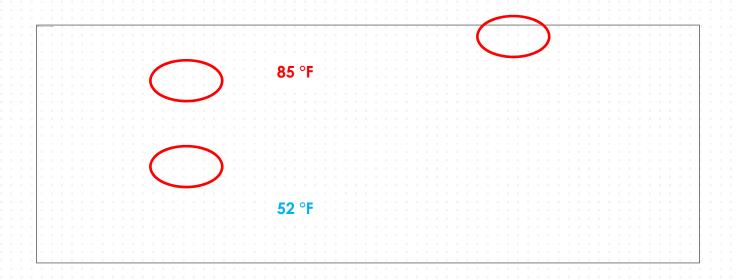
...in other words..

VAV AIRFLOW CONTROL Discharge Air Temperature...



VAV AIRFLOW CONTROL Discharge Air Temperature...

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DAT = [(1,087 CFM / 1808 CFM) * 85° F] + [(721 CFM / 1808 CFM) * 52° F] 71.8° F

MOVING FORWARD...

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AT BAS:

- Repeated DAT calculation (Spreadsheet) for each VAV...
- ...found many VAVs with identical issue.

In Field @ three random VAVs:

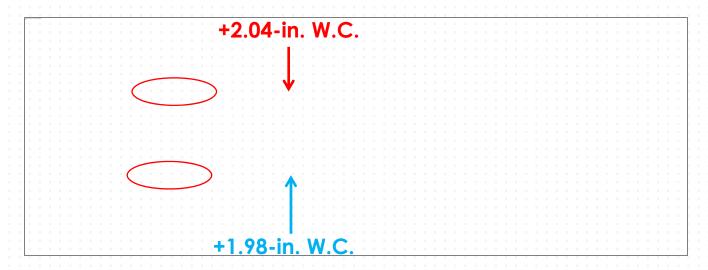
- Verified DAT sensor location; GREAT location!
- BAS Temperature indication within ½° calibrated instrument

FIELD VERIFICATION...

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Actual VAV damper position vs. BAS indication...

...matched...



Measured Hot and Cold Duct inlet pressure...

...pretty high for VAVs without coils...

Tested Airflow at VAV inlets...



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Comparison of data plot on airflow chart (Typical of 3)...

Plotting sensor ΔP on this chart were disturbing...

...actual airflow is NEVER on the curve but in the area between the Maximum & Minimum CFM

VAV AIRFLOW CONTROL Thoughts...Next Steps...

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Just how big was this issue?

Verify airflow for entire AHU...

AT AHU...

- Measure Fan Operational Data (RPM, Volts, Amps, TSP), plot on fan curve and fan tables...
- Traverse Hot & Cold Deck Coils...
 - Shortridge VelGrid at discharge with 6-inch stand-offs
 - Unit free area @ traverse point calculate airflow
- Traverse all Supply Air ducts (4 Hot ducts & 4 Cold ducts)...

VAV AIRFLOW CONTROL AHU CFM vs. BAS CFM

- AHU airflow comparisons...
 - All three sets of airflow data ±2% of one another which is...
 - ...WELL within acceptable instrument error...
- BAS Hot & Cold VAV CFM summary vs. measured CFM:
 - Actual Hot Deck airflow 122% of BAS indication
 - Actual Cold Deck airflow 118% of BAS indication

VAV AIRFLOW CONTROL Points of Energy Saving

- Fan Energy:
- Down-Duct Static AND CFM reduction (VFD or Sheave Change)
 = SIGNIFICANT kW/hour reduction
- Heating Coil Steam load...
 - 100% Outside Air, winter would require significant steam...
- Chilled Water production and distribution costs:
 - 100% OA Sensible & Latent cooling

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...significant energy expenses due to inaccurately calibrated, Pressure Independent VAV Terminal Units.

WHAT TO DO?

- Educate MEP, TAB & Cx Personnel
- Project schedule/completion dates drive project activities instead of logic...
 - Sometimes this works...
 - Other times, it can be catastrophic

WHAT TO DO?

- Educate MEP, TAB & Cx Personnel (contined)
- 2. TAB with incomplete AHU control system cannot be overlooked without consequences.
 - Educated & diligent TAB personnel can overcome this...
 - ...and make it right at the end of the project but...
 - ...this is a LOT of extra work requiring compensation.

WHAT TO DO?

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- Educate MEP, TAB & Cx Personnel (contined)
- 2. NEBB, AABC & TABB Procedural Standards require fully operational control systems to commence TAB activities.

Proceeding with system TAB without completed BAS control compromises the NEBB, AABC & TABB process...

...will compromise the guarantee of accuracy by these bodies which is often paid for by the owners.

WHAT TO DO?

- Educate MEP, TAB & Cx Personnel (contined)
- 3. Calibrate VAV near operational static pressure.
- 4. ALWAYS be aware of hydraulically hardest to satisfy VAV.

WHAT TO DO?

- Educate MEP, TAB & Cx Personnel (contined)
- 5. Cx personnel need to support TAB personnel...
- 6. Cx personnel must educate clients, introduce intelligence into the process, ENERGY LATER vs. Project Schedule gain now.

WHAT TO DO?

Reliable Without Limitations?

BAS Applications for DDC VAVs Need Additional Calibration Capability

7. Most DDC VAV programs reconcile inlet duct airflow sensor ΔP with actual airflow using a form of the algorithm below...

Current CFM = $(\sqrt{\Delta P} \text{ Current}/\Delta P \text{ at Calibration}) * CFM at Calibration * Correction Factor$

8. Add additional calibration points into the VAV application

WHAT TO DO?

Reliable Without Limitations?

Request Publiction of ASHRAE 130-2008, Section 5.6 Test Data

Something is going on, let's hear from the experts!

CONCLUSION

Reliable Without Limitations?

NOT a "Silver Bullet" for energy reduction in every building with pressure independent VAV systems.

DOES represent potential energy waste.

SHOULD be investigated and understood.

Ron Simens rsimens@facilitydynamics.com THANK YOU (831) 206-4489 Commissioning-Controls-Remedial Engineering